



Sandia EB1200 Experiments: ELM Simulations on W Rod Mockups & Thermal Modeling

SNL Contributors:

Dennis Youchison	Jimmie McDonald
Richard Nygren	Fred Bauer
Tom Lutz	Ken Troncosa
Mike Ulrickson	

presented by: Richard Nygren

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Outline

- I. Heat loads for ITER ELMs and capability of EB1200
- II. Initial results from EB1200 experiments on a new W rod mockup made by Plasma Processes, Inc. (PPI)
- III. Thermal modeling of ITER ELMs on W rod armor

Youchison presentation on W rod mockups

Mockup V2-02-15Q

Rods: lanthanated W 3.2mm dia.

Rod Tip: ~2mm, 45° truncated, Ni coating

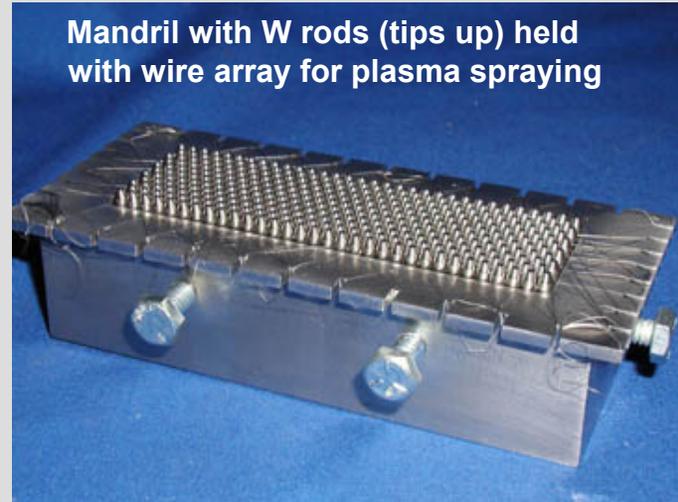
Bed: plasma sprayed CuCrNb (1mm)

Armor: 5 mm high, 32 x 95 mm

Heat Sink: CuCrZr, E-beam welding

Cooling: 10 mm dia. channels (2),
water cooling, twisted tape insert (tt=2)

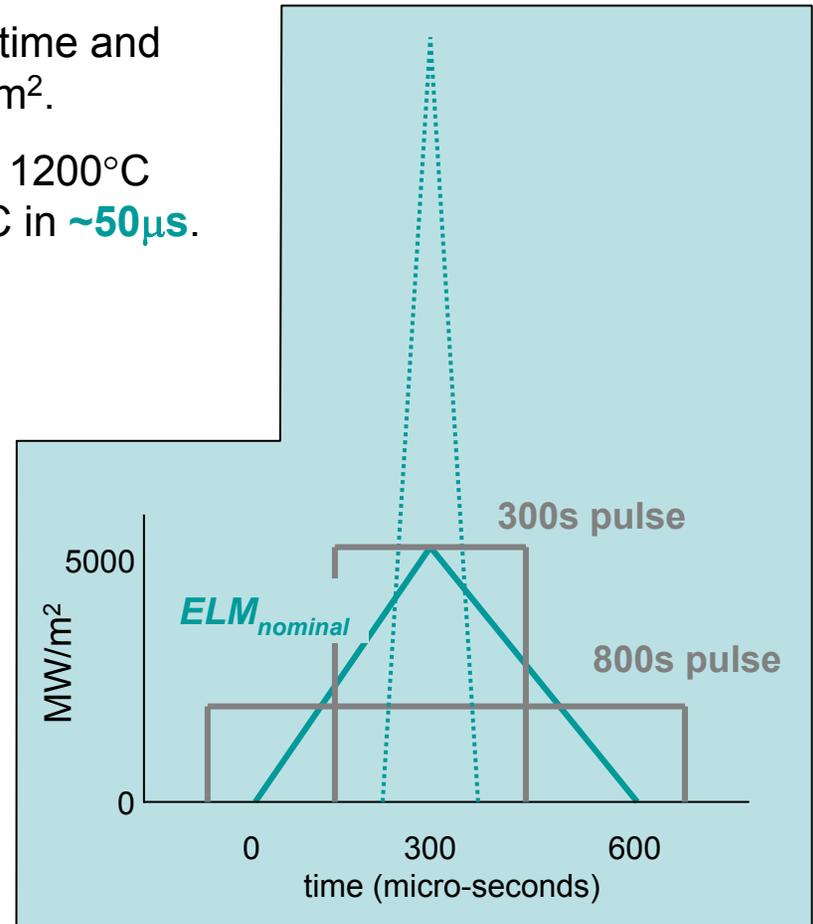
Mandril with W rods (tips up) held
with wire array for plasma spraying



ITER ELMs will loose 12 MJ of energy (12% $E_{pedestal}$) from the plasma in $\sim 200 \mu s$.

A. Loarte et al., "Predicted ELM Energy Loss and Power Loading in ITER-FEAT," IAEA Meeting

- The nominal "ITER ELM" has 300 μs rise time and 300 μs fall with a 5000 MW/m² peak for 8m².
- For $q'' = 5000 \text{ MW/m}^2$, tungsten initially at 1200°C reaches its melting temperature of 3377°C in $\sim 50 \mu s$.
- The integrated power density can be represented by square pulses:
 - 5000 MW/m² for 300 μs or
 - 1900 MW/m² for 800 μs .

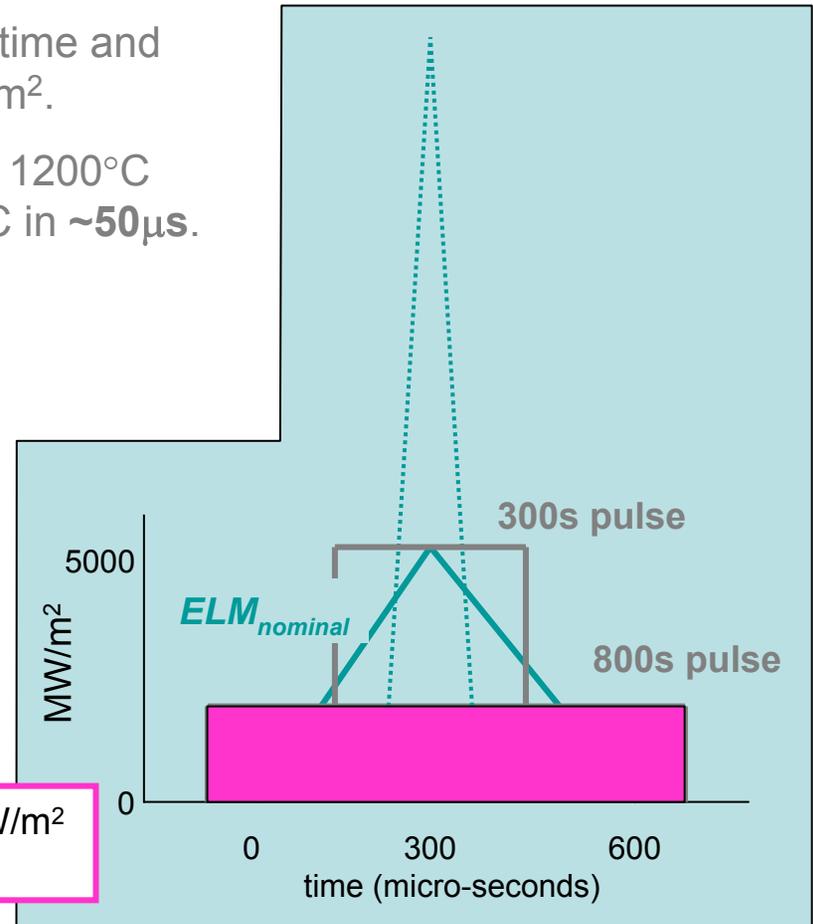


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- The integrated power density can be represented by square pulses:
 - 5000 MW/m² for 300 μs or
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- Cases with deposition areas of 8 or 16m² and times of 100-300 μs were analyzed.
- Mitigation of ELM heat loads is an area of active study.

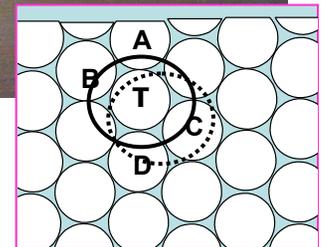
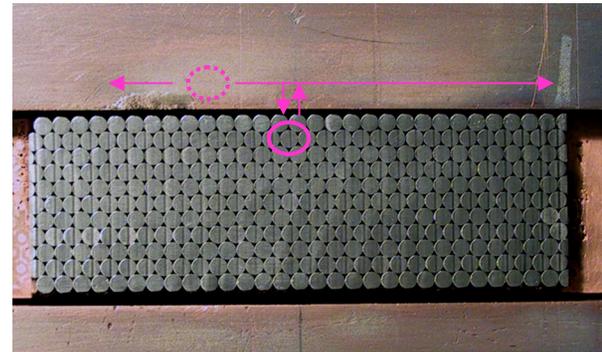
- Our tests investigate heat loads of 1000-2000 MW/m² and times of 300 and 800 μs .



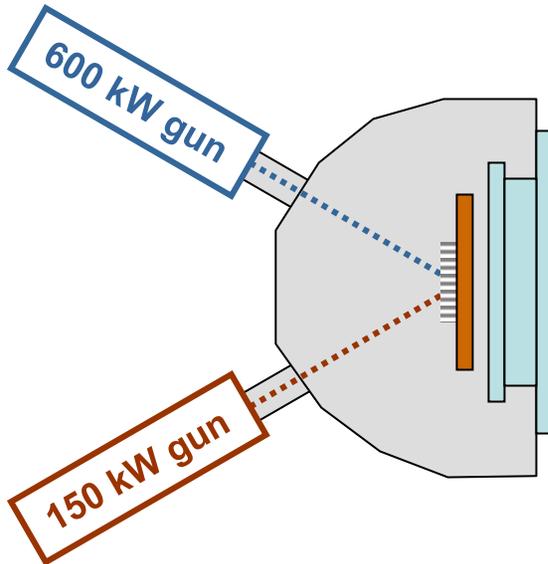
EB1200 can pause the beam spot for pulses of $\sim 200\mu\text{s}$.

EB1200:

- Youchison's digital rasting system maps the beam pattern in a series of discrete spots.
- Restoring frequency (coils) is 10kHz max. Minimum "spot" time is $\sim 100\mu\text{s}$.
- A reasonable minimum is 200-300 μs when we move onto and off a target.
- We can tell if a spot is aligned on the target rod (T) by looking at the temperatures of the surrounding rods.



We will use a “two gun” approach.



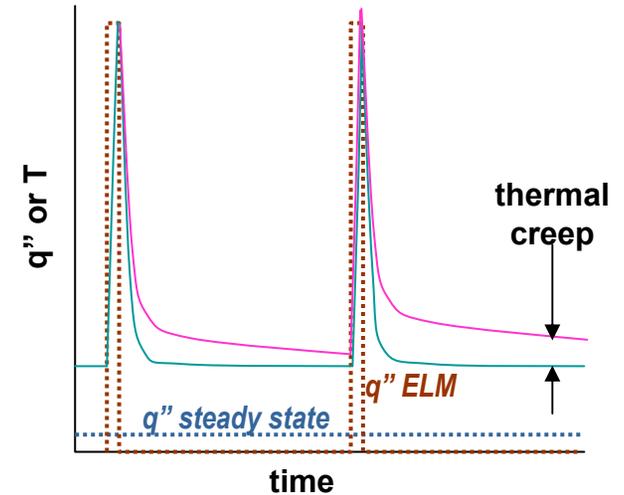
Procedure:

- Maintain a **steady surface temperature** on the mockup with the 600 kW gun.
- Move the defocused beam from the 150 kW gun* from a sweep pattern on the shield to a target W rod for a **300 or 800 μs “ELM”** and then back to the shield.
- Measure the temperature of a target W rod with a **fast IR pyrometer at 10 μs frame**.
- Monitor the mockup with **pyrometers, TCs, IR camera, and water calorimetry**.
(30 Hz IR frames can give some data on “tail.”)
- Compare results with **thermal modeling**.

*With its smaller beam spot of ~ 2 mm diameter, the 150 kW gun can give a higher heat load on an individual rod than the 600 kW gun. With the spot is defocused to a 4 mm diameter, we expect a maximum q''_{absorbed} of ~ 4.1 GW/m² with 60% reflected power and an incident angle of 60°.

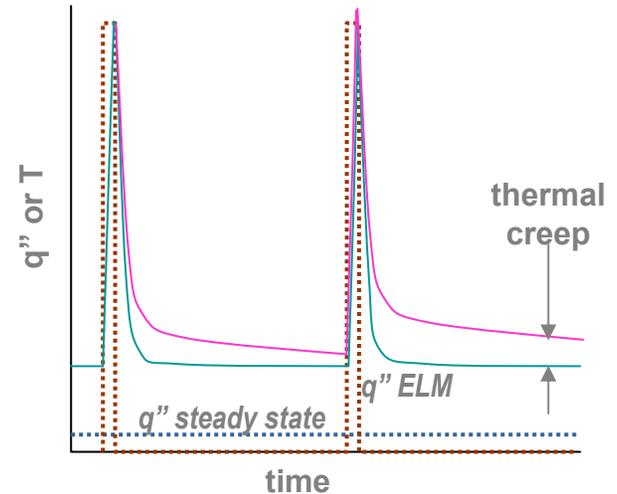
“Thermal creep” from repeated ELMs is a key factor.

- ITER’s estimated ELM frequency is 2-5 Hz.
- Initially, thermal penetration is very shallow.
- An assumption that ELMs produce only a surface perturbation is dangerously wrong!
- We see a significant tail in the cooling curve in the modeling and experimental results.



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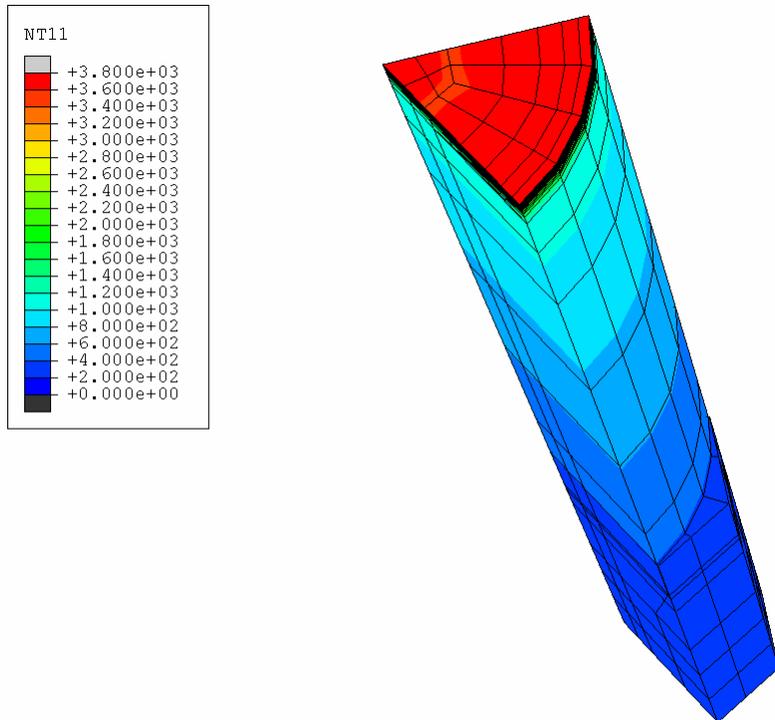


Major objectives include measuring the following:

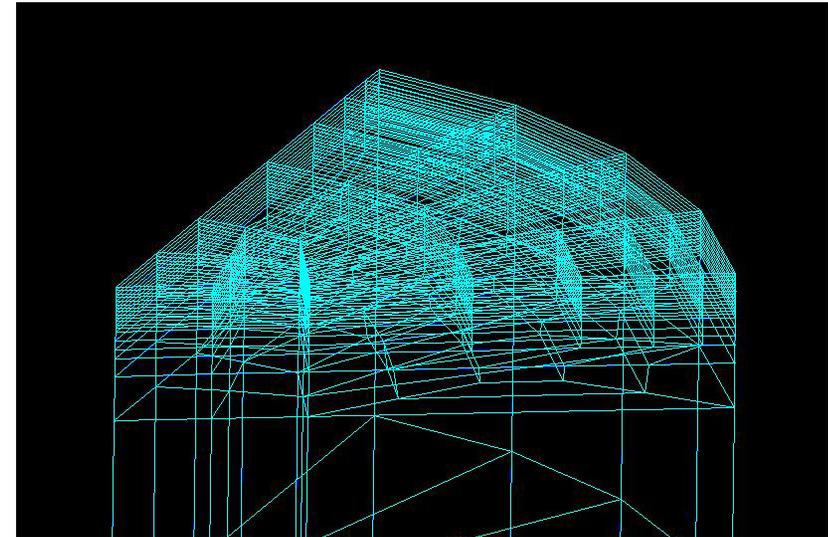
- **ELM power to initiate melting** (varies with the starting temperature)
- **T_{surface} vs. time** (including “**thermal tail**”) for various ELM heat loads.
- **Response to repeated ELMs** (thermal creep, i.e., increasing T_{surface} with cycles.
- We just began testing (shakedown) with heat fluxes up to **$\sim 14\text{MW/m}^2$** .
- We have **no “ELM” data yet.**

Initial 3-D model too coarse.

This model is was modified from one used for steady state thermal analysis.

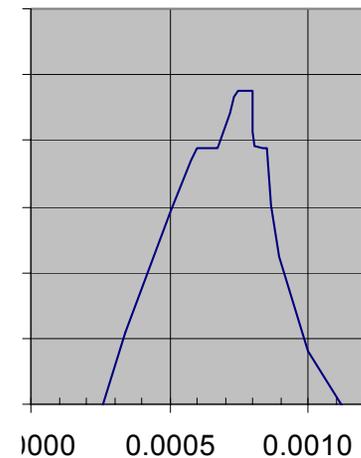
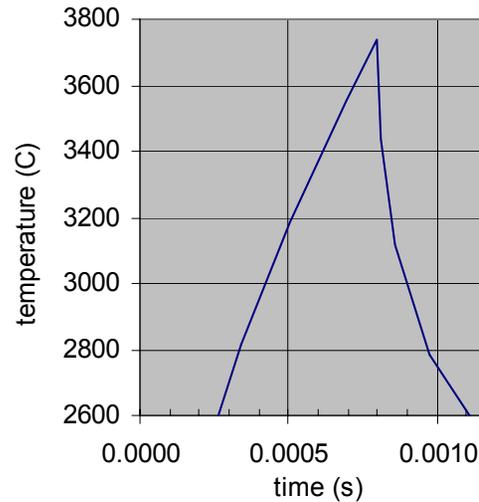


ABAQUS job created on 29-Jan-04 at 15:32:54
OBJ: elm15q10p8t140.oab ABAQUS/Standard 6.4-1 Mon Mar 29 11:24:59 Mountain St
Step: Step-2
Increment 159: Step Time = 8.0000E-04
Primary Var: NT11
Deformed Var: not set Deformation Scale Factor: not set



elm15q10p8t140 - no latent heat

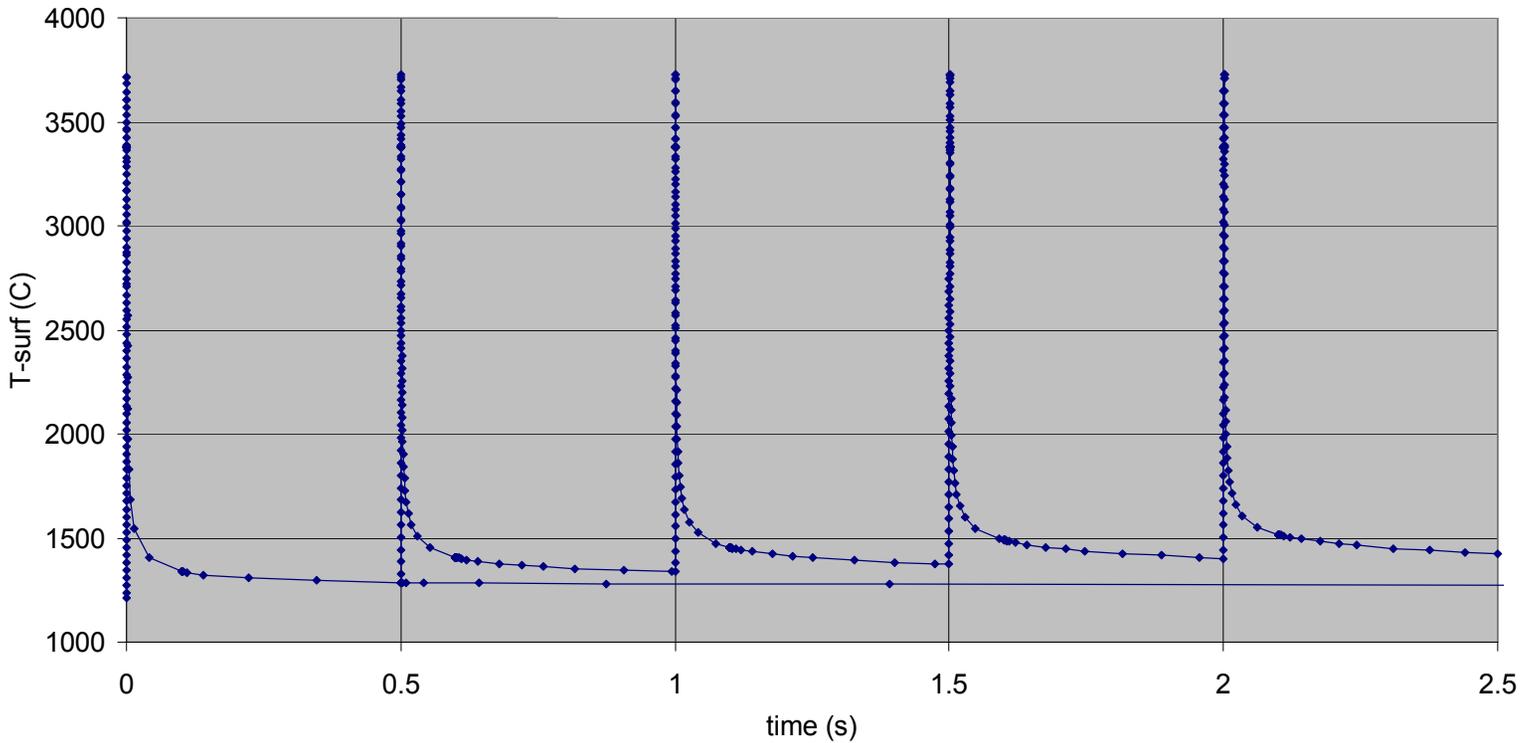
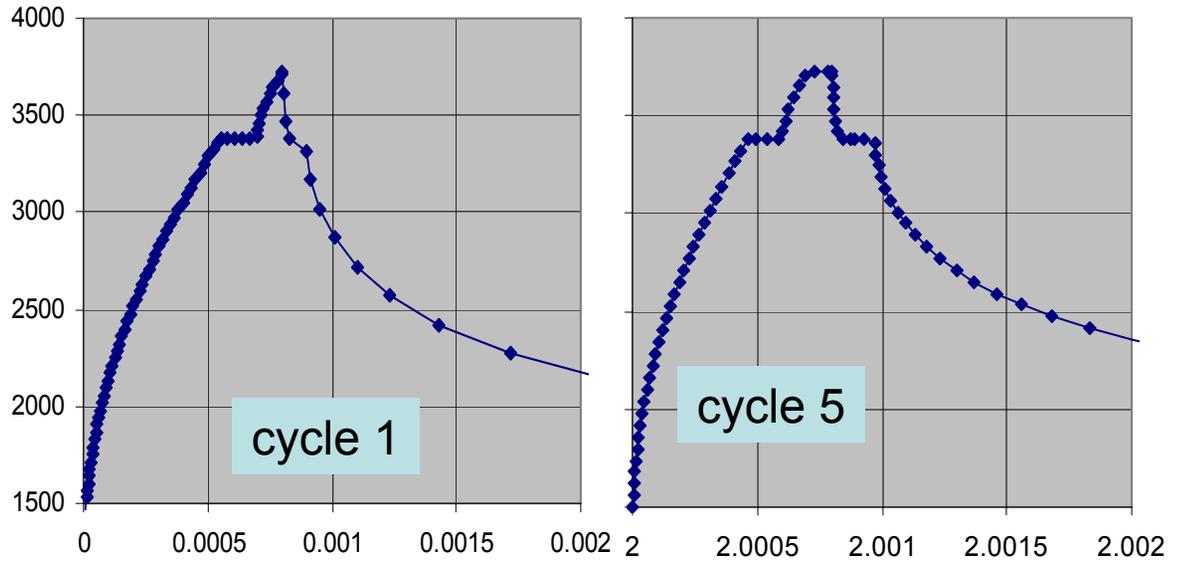
with latent heat



First 2-D model

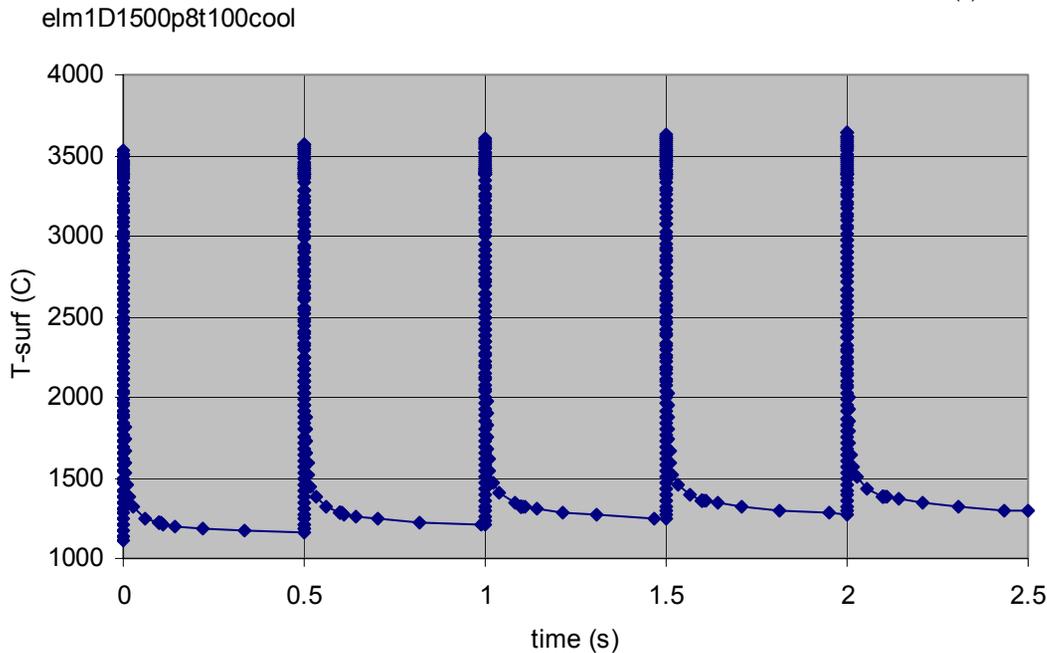
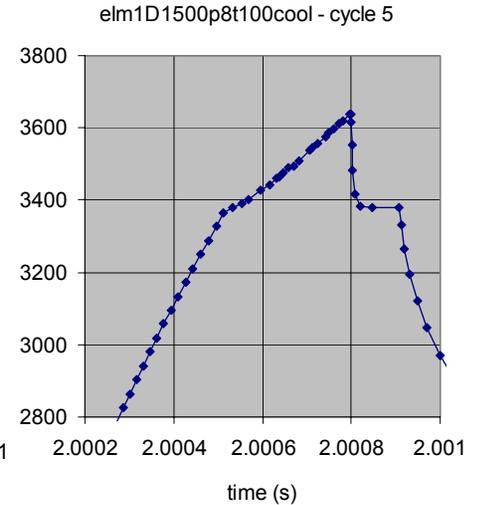
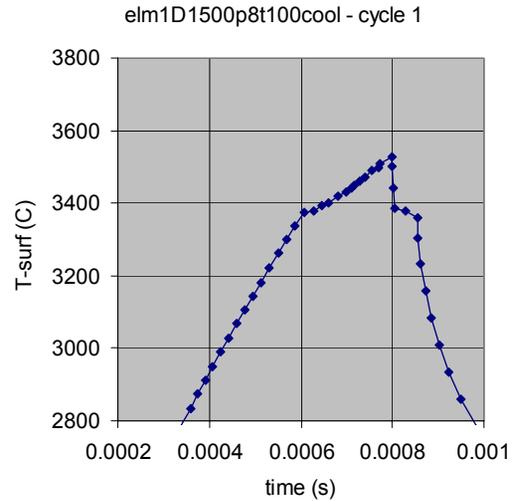
- Still too coarse.
- But thermal creep is evident.

elm2D1500p8t100cool2Hz



1+D model works.

- No apparent problem with discrete layers.
- Thermal creep is significant.
- Case: 1500MW/m² 800μs
2Hz (~1 of 10 points plotted)

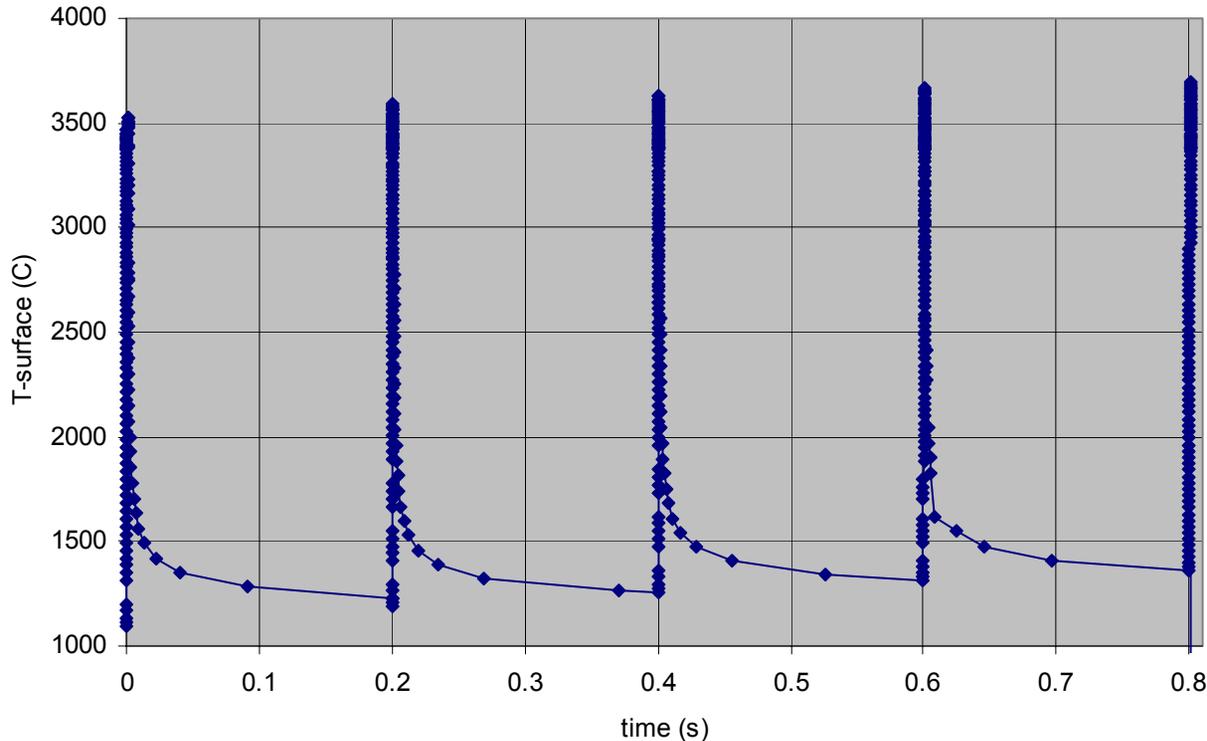


cycle	T _{peak} (C)	T _{start} (C)
1	1161	1112
2	1210	1182
3	1246	1230
4	1274	1267
5	1295	1294

1+D model case: 1500MW/m² 800μs 5Hz

- Thermal creep is greater (as expected) than for 2 Hz case.
- First pulse to pulse increase is ~95°C.
- This decreases to ~48 °C on 5th pulse.

elm1D1500p8T100cool 5Hz



cycle	T-peak (C)	T-start (C)
1	3528	1091
2	3588	1186
3	3632	1254
4	3664	1310
5	3695	1358

Summary

- Initial thermal analyses suggest that repeated ELMS will increase the surface temperature of PFC armor in ITER.
- We have demonstrated the capability of EB1200 to produce ELM-like heat loads on a target W rod in a W rod mockup.
- We anticipate having initial experimental data to include in our PSI paper on ELM testing.

“Simulation of ELMS in HHF Tests of W Rod Armor”

**R.E. Nygren, D.L. Youchison, M.A. Ulrickson,
J.M. McDonald, and T.J. Lutz**