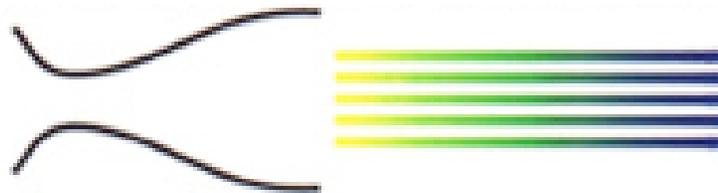


# Plasma Facing Component Development at PPI

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**Scott O'Dell**  
**Plasma Processes, Inc.**

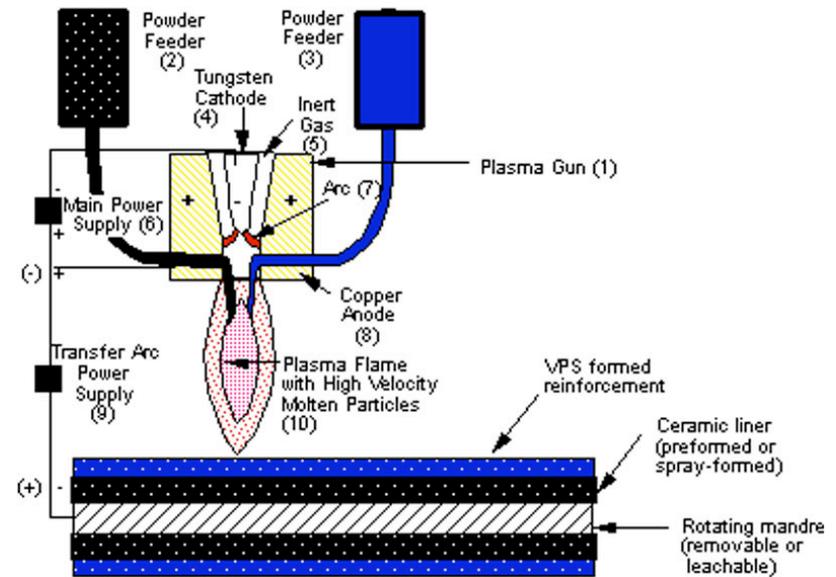


PFC Spring Meeting  
University of Illinois at Urbana-Champaign  
May 3-5, 2004



# Background

- Plasma Processes, Inc. is a small business that specializes in the development and fabrication of coatings and near-net-shape spray formed structures using Vacuum Plasma Spray (VPS) forming techniques.





## Advantages of VPS Forming Techniques

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- Processing of oxygen sensitive materials
- Ability to use reactive gases
  - H<sub>2</sub> for O<sub>2</sub> reduction
  - N<sub>2</sub> for nitriding
- High temperature plasma enable processing of high melting temperature materials
  - Refractory metals (e.g., W, Re, Mo, Ta, Nb)
  - Ceramics (Al<sub>2</sub>O<sub>3</sub>, Y<sub>2</sub>O<sub>3</sub>, HfN)
  - Carbides (e.g., TaC, HfC)
- CNC control enables contour following and uniform, repeatable deposition thicknesses
- High deposition rates (e.g. >10kg/hour)
- Deposition of alloys and dispersion strengthened materials
- Net shape (near) spray formed components using removable mandrels
- Post-spray heat treatments can result spray formed materials with density >99% and properties equivalent to or exceeding wrought materials
- Ability to tailor the structure of the deposits by varying the spray parameters
  - Porous structures
  - Functional gradient layers for joining materials with dissimilar CTEs
  - Multi-layered structures



# PFC Development

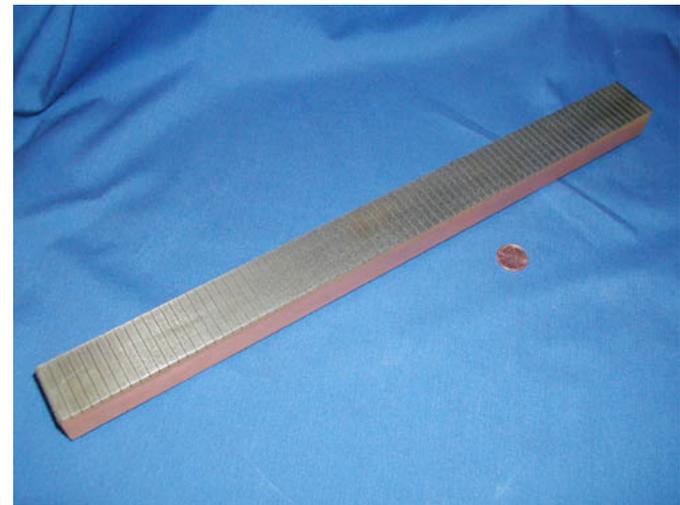
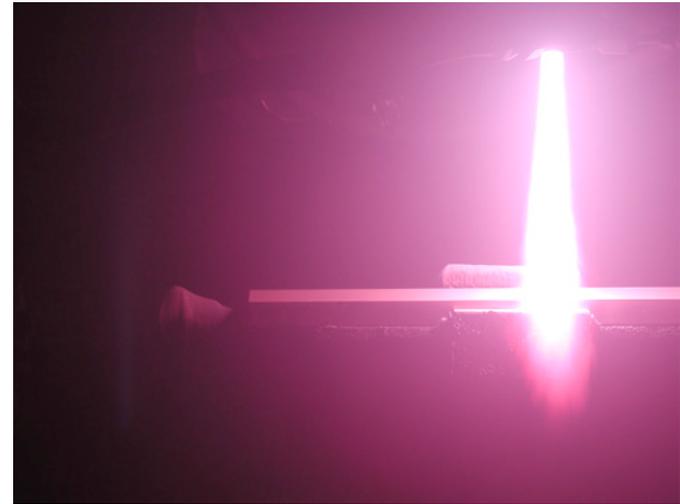
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- Armor
  - VPS W and Be
  - W and Be brush
- Spray Formed Refractory Metal Heat Sinks
  - Liquid Metal Cooled
  - He Cooled
- Engineered Materials
  - Nanograined W
  - Nanoporous W armor for laser IFE



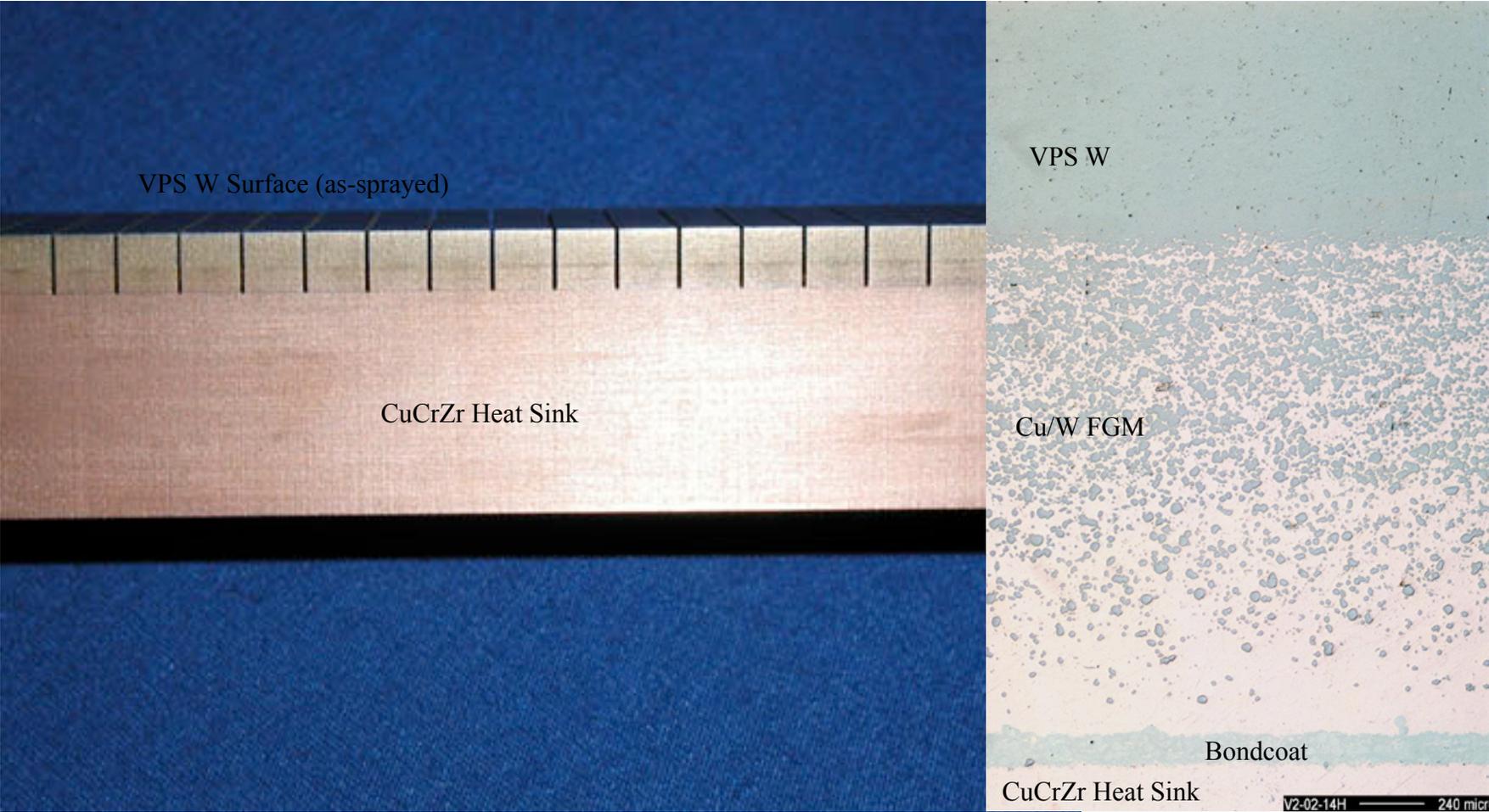
## VPS Armor on Cu Alloy Heat Sinks

- Ar/H<sub>2</sub> Plasma
- Rectilinear pattern
- CuCrZr heat sink
  - 400mm length x 40mm width
- Cu/W functional gradient to reduce stress due to CTE mismatch
  - W:  $4.4 \times 10^{-6}/K$
  - Cu:  $16.8 \times 10^{-6}/K$
- 2mm gradient enabled the VPS deposition of 5mm thick W deposits
- After deposition, width trimmed to 32mm and armor castellated





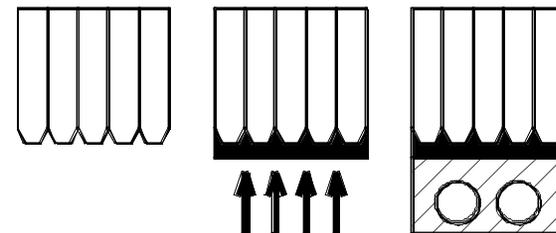
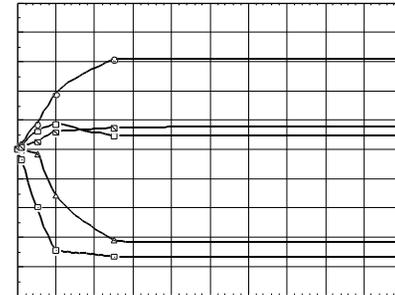
# VPS W Armor on a CuCrZr Heat Sink





# Brush Armor

- SNL showed by reducing the tile width the stress at the tile/heat sink interface can be reduced
- Using preformed W and Be rods, a VPS backing material is deposited on the tips of the rods
  - Fine grain microstructure
  - Ability to apply bondcoats or diffusion barriers
  - Minimal penetration of backing material down the rod length
- Backing material is then joined to CuCrZr heat sink using HIP diffusion bonding or deep penetration electron beam welding





## HHF Testing of Brush Armored Mockups

ID Number	Heat Sink (Channel)	Backing Material	Bond Coat	Rod/Tip Configuration	Dam	Armor Height, Width and Length (mm)*	Armor to Heat Sink Bonding
PW-4	Cu alloy (Single)	Cu (1mm)	Ni	W (1.6 mm dia.) 45° pointed	Inconel	10 x 16 x 70	HIP diffusion
PW-10	CuCrZr (Single)	Cu (3mm)	Ni	W (3.2 mm dia.) 45° truncated	Inconel	10 x 16 x 65	E-beam
PB-9	Al 6061 (Single)	Al (3mm)	None	Be (2 x 2mm square) 45° pointed	None	5 x 17 x 65	E-beam
PW-8	CuCrZr (Dual)	Cu (1mm)	Ni	W (3.2 mm dia.) 45° truncated	Inconel	8 x 32 x 102	HIP diffusion
PW-14	CuCrZr (Dual)	Cu (2mm)	Ni	W (3.2 mm dia.) 45° truncated	Inconel	8 x 32 x 102	E-beam
PW-14b	CuCrZr (Dual)	Cu (2mm)	Ni	W (3.2 mm dia.) 45° truncated	Inconel	8 x 32 x 102	E-beam



- W brush armored, dual channeled mockups have survived  $>20\text{MW/m}^2$  for 500 cycles and thermal response heat fluxes  $>25\text{MW/m}^2$
- Be brush armored mockups have survived HHF testing at  $5\text{MW/m}^2$  for 353 cycles

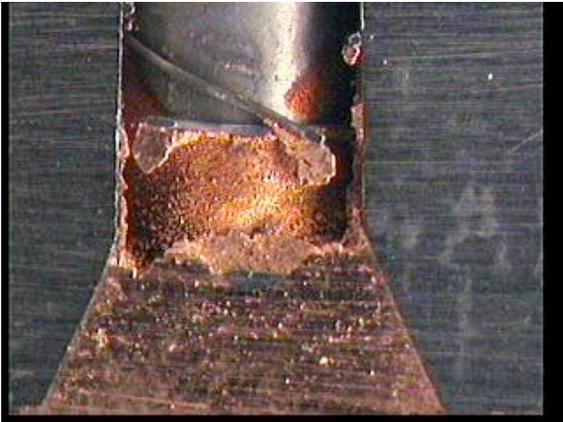
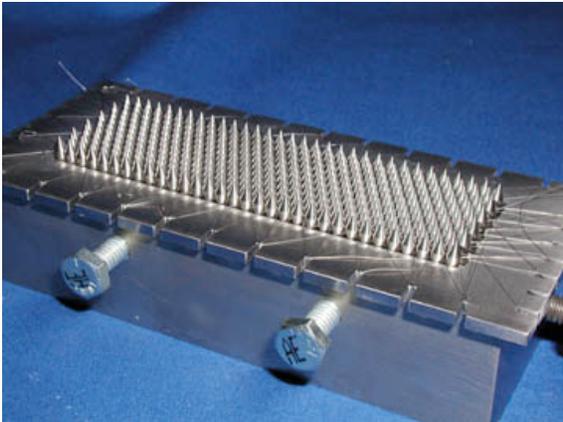
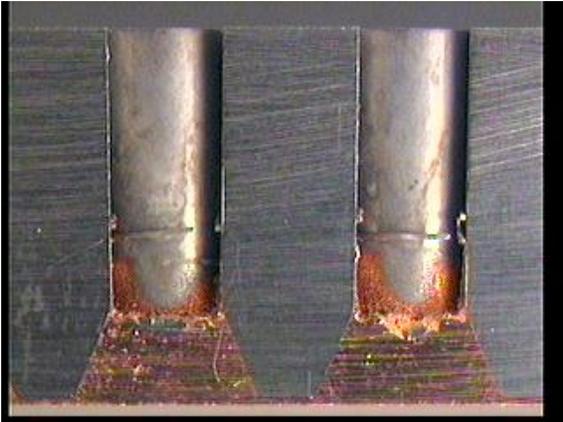
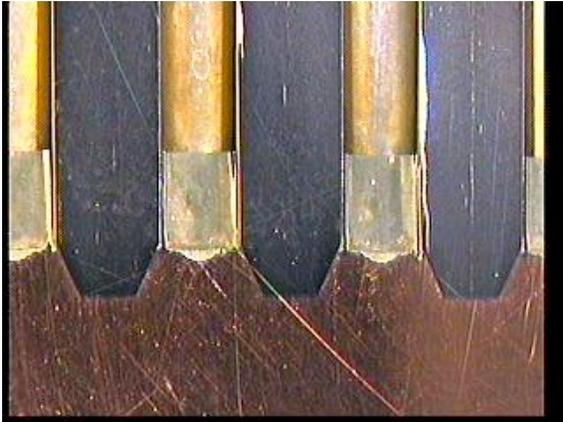


## 2<sup>nd</sup> Generation of W Brush Armored, Dual Channeled Mockups

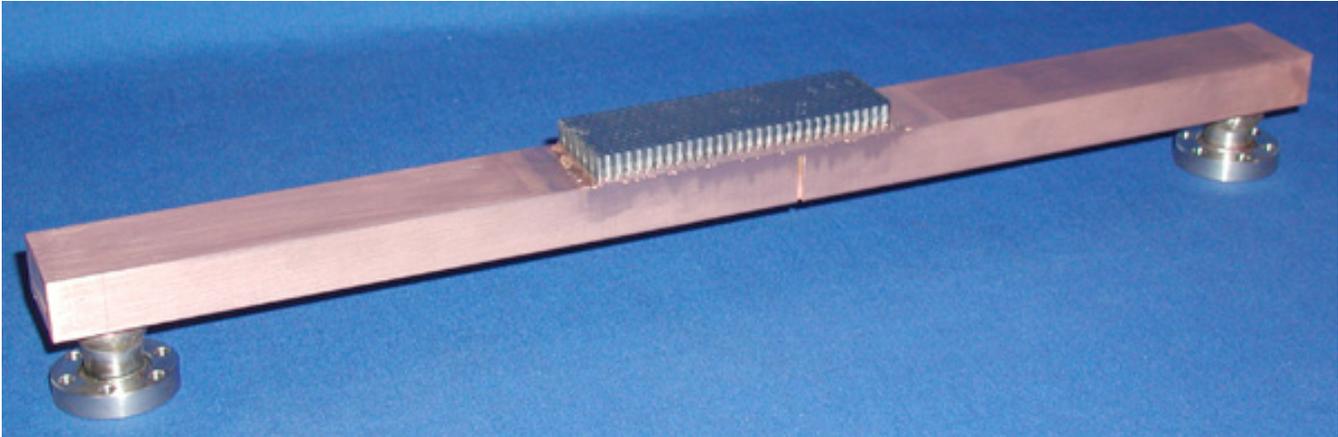
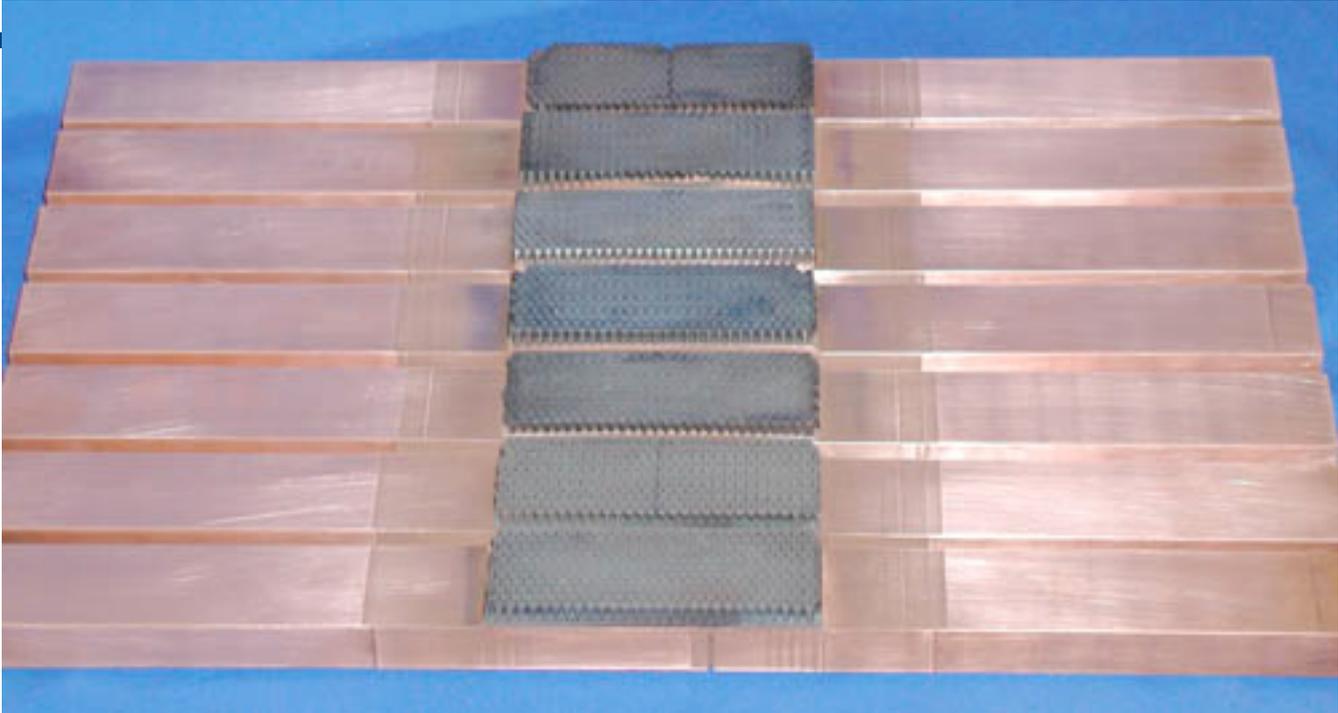
ID Number	Heat Sink (Channel)	Backing Material	Bond Coat	Tip Configuration	Dam	Armor Height, Width and Length (mm)	Armor to Heat Sink Bonding
V2-02-15B	CuCrZr (Dual)	Cu (1mm)	Ni	W (3.2 mm dia.) 45° truncated	W wire (100_m)	5 x 32 x 95	HIP diffusion
V2-02-15F	CuCrZr (Dual)	Cu (1mm)	Ni	W (3.2 mm dia.) 45° pointed	W wire (100_m)	5 x 32 x 95	HIP diffusion
V2-02-15K	CuCrZr (Dual)	Cu (1mm)	Ni	W (3.2 mm dia.) 45° truncated	None	5 x 32 x 95	HIP diffusion
V2-02-15N	CuCrZr (Dual)	Cu (1mm)	None	W (3.2 mm dia.) 45° truncated	W wire (100_m)	5 x 32 x 95	HIP diffusion
V2-02-15S	CuCrZr (Dual)	CuCrNb (1mm)	Ni	W (3.2 mm dia.) 45° truncated	W wire (100_m)	5 x 32 x 95	HIP diffusion
V2-02-15T	CuCrZr (Dual)	CuCrNb (1mm)	Ni	W (3.2 mm dia.) 45° truncated	W wire (100_m)	5 x 32 x 95	HIP diffusion
V2-02-15Q	CuCrZr (Dual)	CuCrNb (1mm)	Ni	W (3.2 mm dia.) 45° truncated	None	5 x 32 x 95	E-beam welding
V2-02-15R	CuCrZr (Dual)	CuCrNb (1mm)	Ni	W (3.2 mm dia.) 45° truncated	None	5 x 32 x 95	E-beam welding



# Honeycomb dam vs. W wire dam



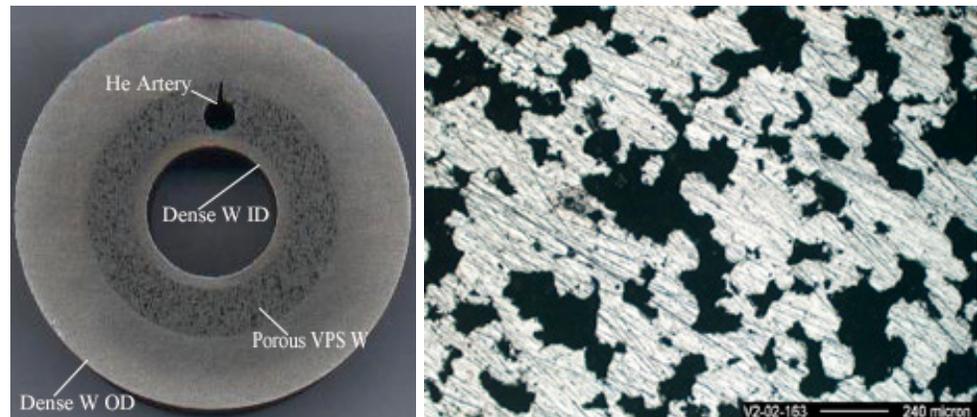
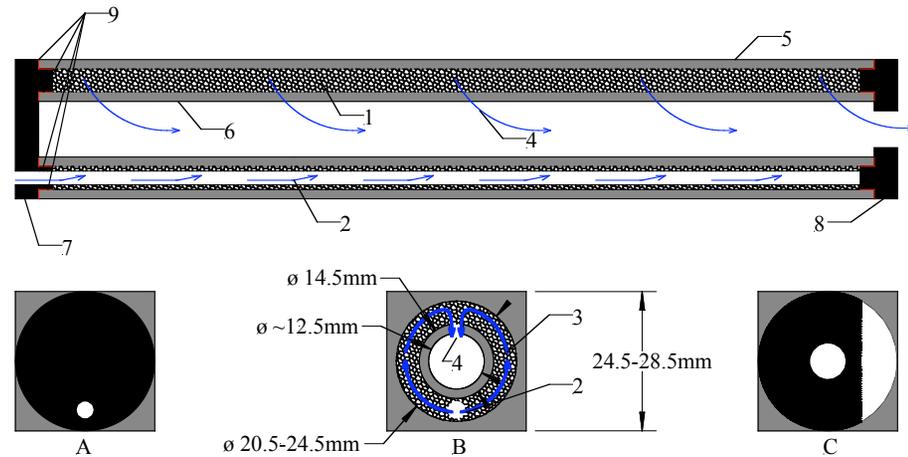
Plasma Processes, Inc.





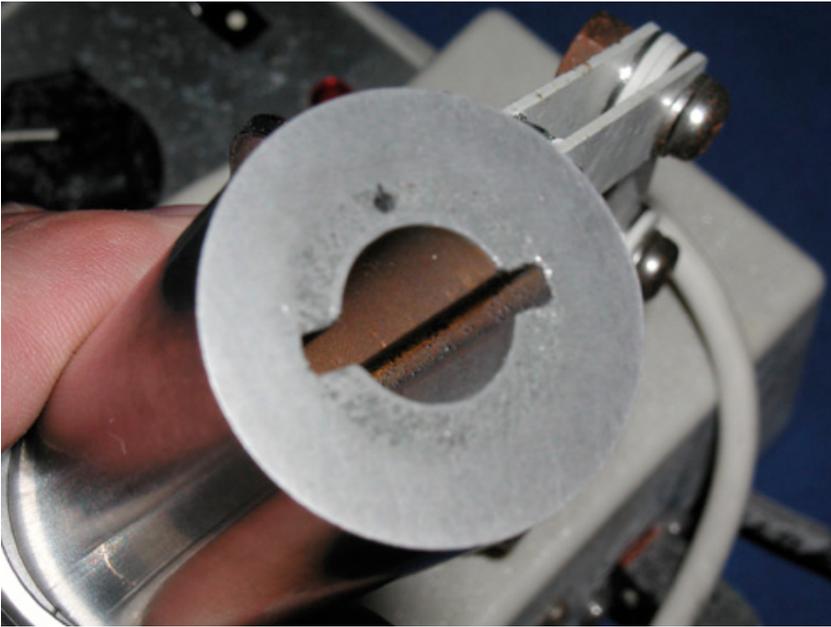
# He Cooled Refractory Metal Heat Sink

- Using removable mandrels and by controlling the deposition parameters, porous W deposits between dense W layers have been produced for use as helium cooled heat sinks.
- Porosity levels between 30-70% have been produced.
- Helium flow tests have demonstrated the porosity is interconnected.
- Size of porosity is dependent on the size of the starting powder.





# Spray Formed He Heat Sinks

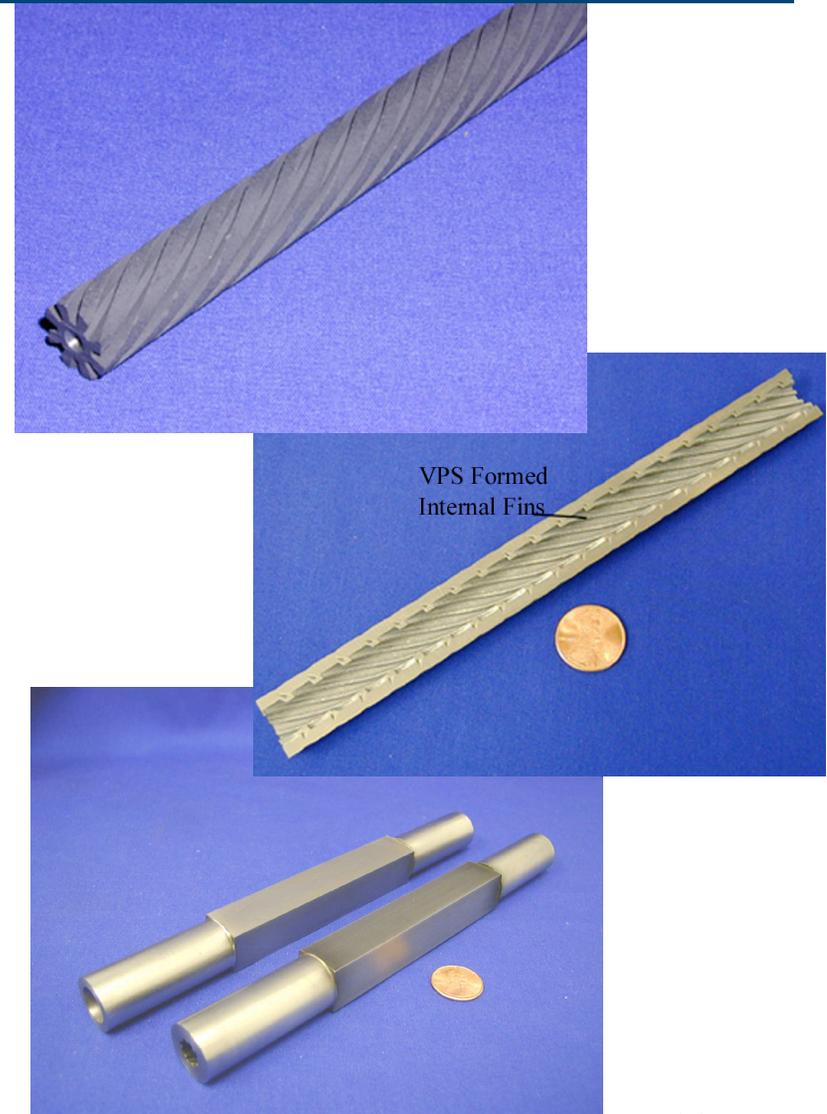




## Liquid Li Cooled Refractory Metal Heat Sinks

- Plasma facing component heat sinks with in-situ formed helical fins
- Machining of the negative configuration into a removable mandrel

ID Number	Material	Bore Configuration
V2000-20	W-Ni-Fe	Smooth
V2000-23B	W-Ni-Fe	Finned
V2000-3C	Molybdenum	Smooth
V2000-24	Molybdenum	Finned
V2002-12D	Tungsten	Finned





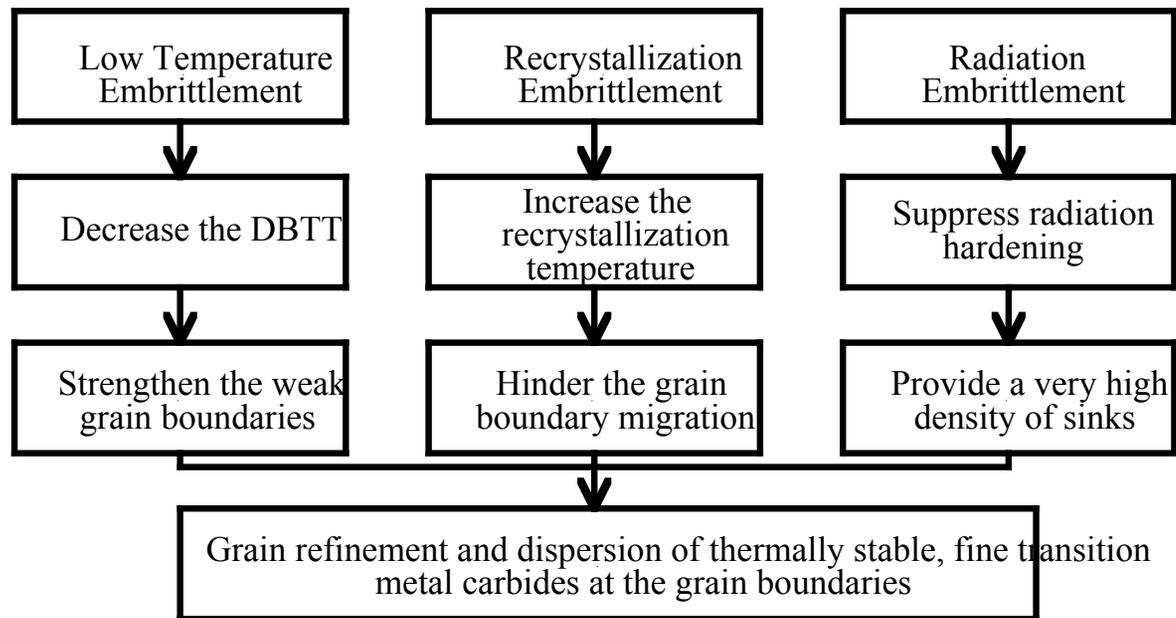
# Liquid Li heat sinks after machining of TC holes and attachment of SS fittings





# Nanograined W for Improved Resistance to Embrittlement

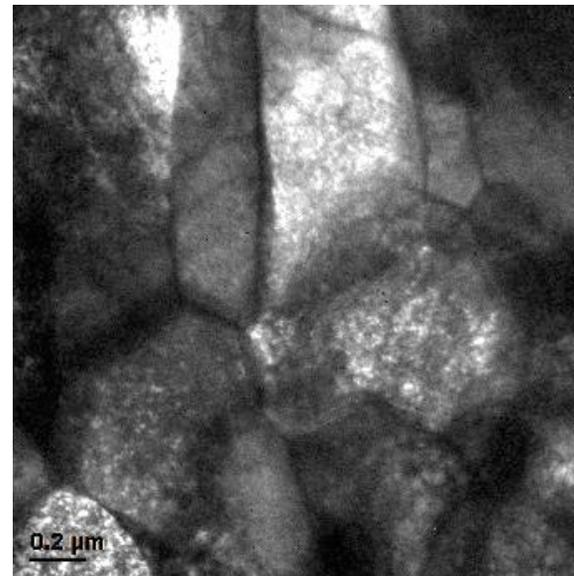
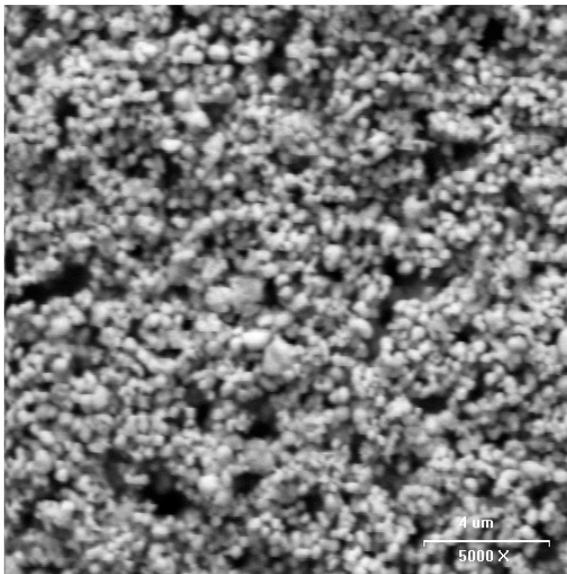
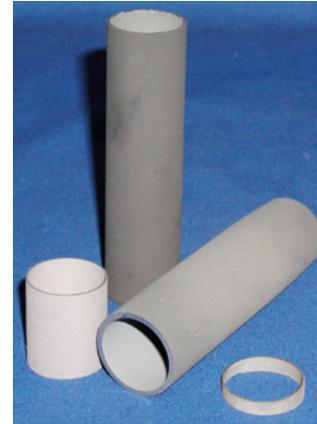
*Prof. Kurishita of Japan identified the benefits of modifying W and Mo with transition metal carbides to achieve fine grain sizes. Potential benefits are improved ductility and resistance to embrittlement.*





## Fabrication of Nanograined W

- Submicron W powder ( $<0.5 \mu\text{m}$ )
- Transition metal carbides to pin the grain boundaries (HfC)

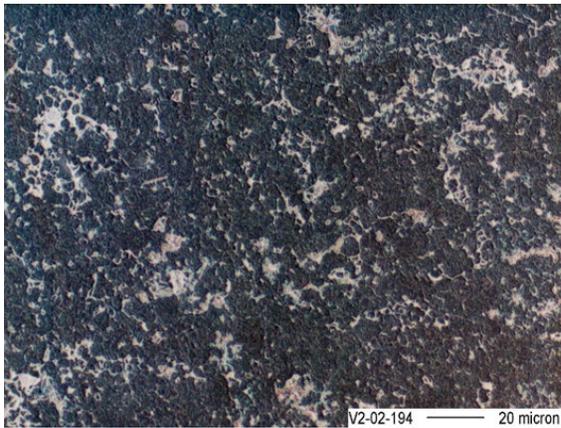




# Effect of high temperature exposure on grain size for samples with and without HfC

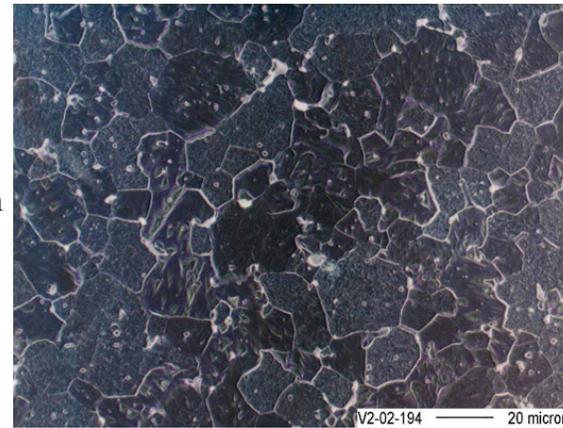
1750°C, 24hrs

W (.5)  
GS: 3\_m

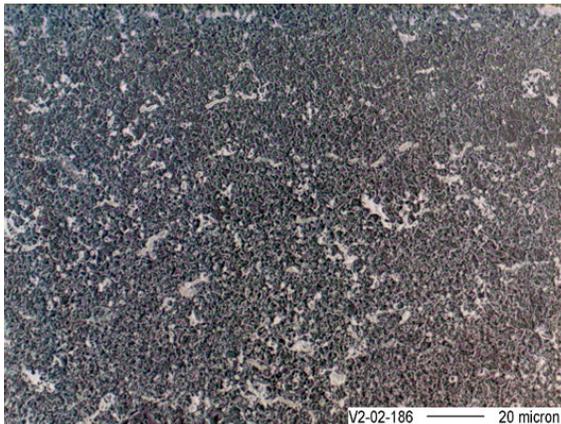


2300°C, 4hrs

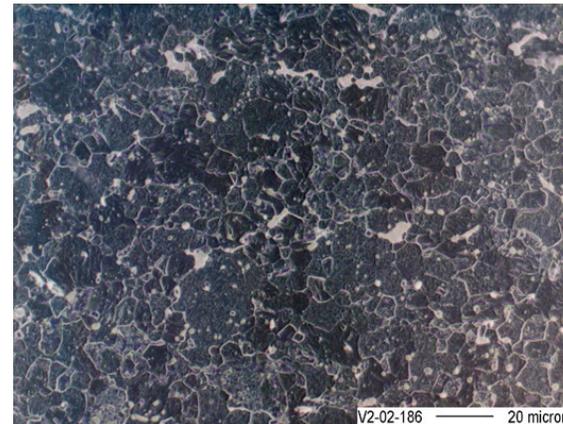
W (.5)  
GS: 11\_m



W (.5)-HfC  
GS: <1\_m



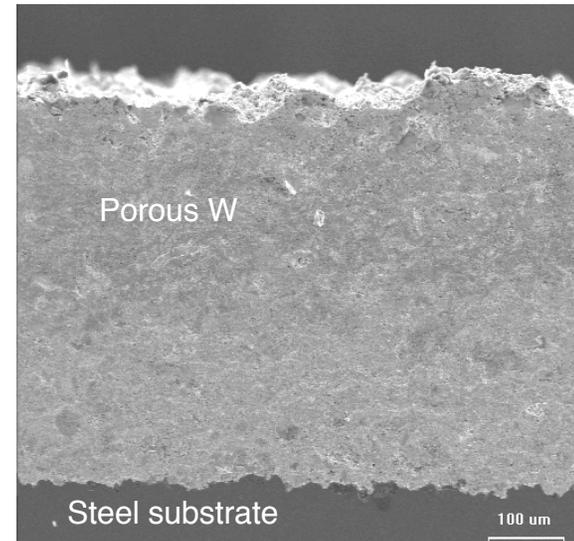
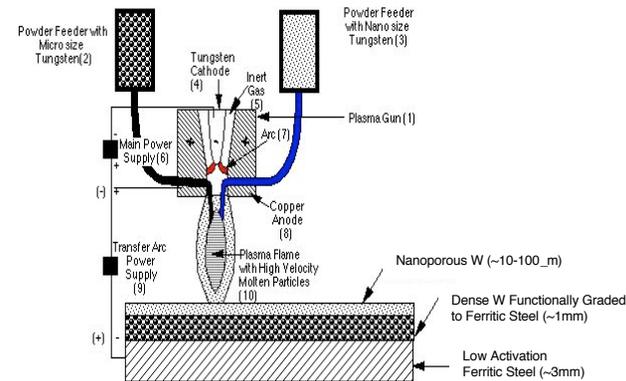
W (.5)-HfC  
GS: 5\_m





## Nanoporous W Deposits on Steel Substrates for Laser IFE

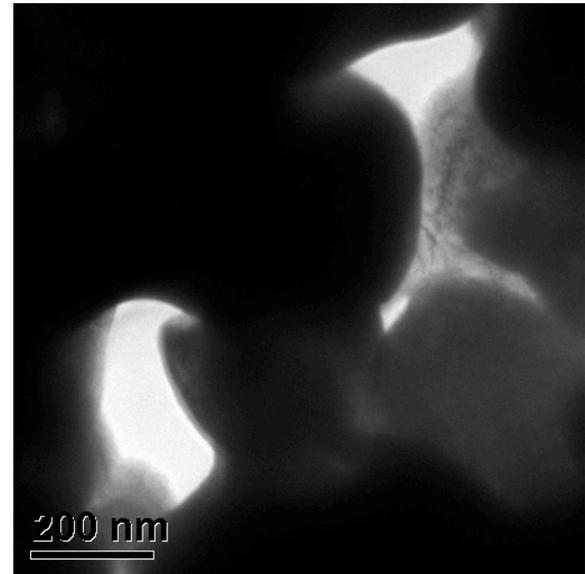
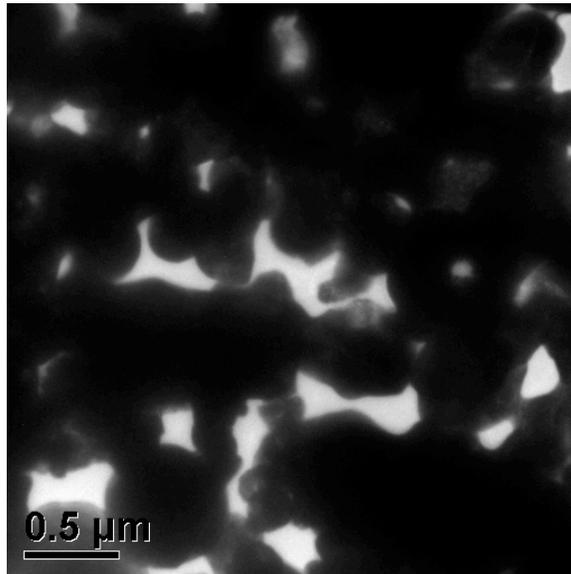
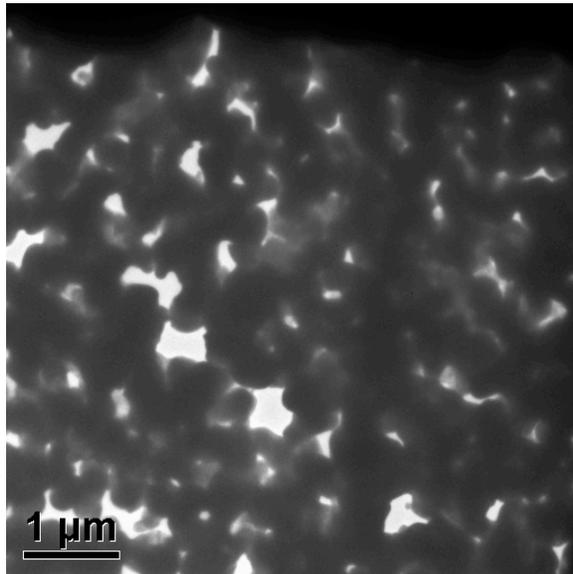
- Steel substrates (25mm x25mm x 5mm)
- Coating thickness: 0.1-1.5mm
- By controlling the heat input to the individual particles, porosity values: 10-30%



SEM backscattered image of a porous tungsten deposit on a steel substrate



## TEM Analysis of Porous Structure



- Bulk density is  $\sim 80\%$
- Distance between pores is  $\sim 500\text{nm}$
- Testing verified the samples are permeable to He



# Summary

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- VPS forming techniques can be used to deposit armor materials on various substrate materials.
- Brush armored mockups have survived cyclic HHF testing at  $>20\text{MW/m}^2$ .
- Components can be produced with tailored microstructures
  - Grain size
  - Porosity
  - Alloys
  - Dispersion strengthened
  - Multiple layers